

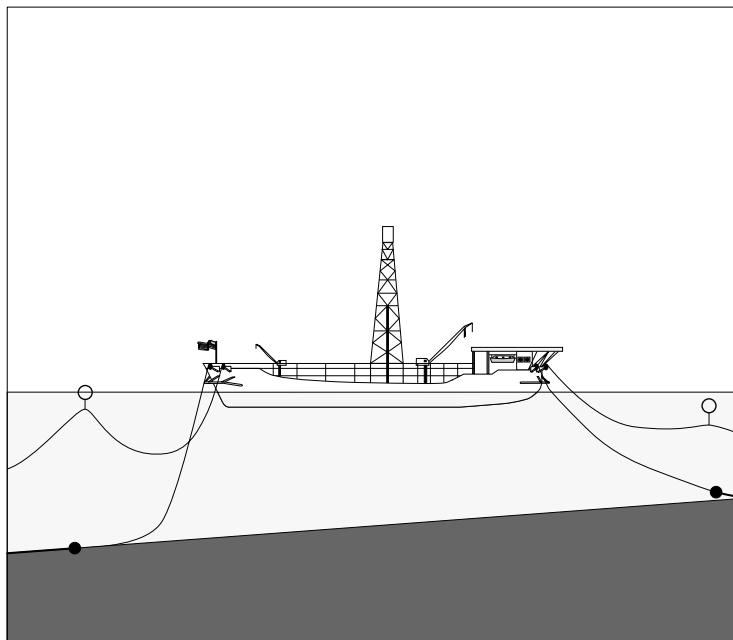
*Introducing*

# Statmoor™

*A Mooring Statics Calculator*

*from*

*SeaSoft® Systems*



*Program Description and Capabilities*

*June, 1989*

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## Executive Summary

**Statmoor** is a state of the art static mooring analysis program developed by SeaSoft Systems and Richard J. Hartman, Ph.D. It is the outcome of the initial phase of a comprehensive mooring system analysis project undertaken in January 1982. Highlights of selected program features follow:

- **Elasticity**

An analytically exact treatment of mooring line elastic deformation allows accurate analysis of the steadily growing family of highly compliant synthetic materials in mooring systems. Commonly employed approximations to elastic deformation in mooring problems can in some cases lead to errors of 100% in restoring force predictions. The exact solution used in **Statmoor** avoids altogether the problem of approximating the effects of either gravity or elasticity in mooring materials.

- **Bottom Friction**

The effect of bottom friction on mooring line tensions in a weakly dynamic environment is shown to be most realistically represented by averaging a double valued tension function.

- **Capabilities**

**Statmoor** can analyze up to 24 mooring lines (12 on microcomputer versions). Each line can consist of 3 sublines including concentrated weights and/or buoys. The ocean bottom may be uniformly sloping or anchor depths can be independently specified. Zero-offset fairlead pretension, distance to anchor or line declination angle can be used to define pretension conditions. English or Metric units may be selected.

- **Versatility**

**Statmoor**'s flexibility makes it useful in non-conventional applications including analysis of rubber hoses used in subsea production, composite towlines, TLP's, guyed towers, tethered buoys and SALMS.

- **Usability**

A powerful user interface provides a simple question-and-answer environment for preparation and editing of input files. No knowledge of computer programming is required. Special built-in *Help* facilities can supply default values for most mooring line material properties or assistance in computing values from user-supplied data.

- **Access**

**Statmoor** is available on an unlimited-use basis through a license agreement with SeaSoft. **Statmoor** is presently configured to run on many popular mini- and microcomputers. In addition, individual timesharing accounts can be set up. **Statmoor** can be configured to run on any computer system possessing a suitable Fortran 77 compiler.

## I. Introduction

**Statmoor** is a state of the art static mooring analysis program developed by Richard J. Hartman, Ph.D. It is the outcome of the initial phase of a comprehensive mooring system analysis project undertaken in January 1982.

In developing **Statmoor**, special attention was given to a number of areas in which at least some of the more well known codes are deficient. The most notable of these areas is the treatment of elasticity of mooring elements. Many modern mooring materials, in particular the synthetics (Kevlar, nylon, polypropylene, etc.), are notable in that their gravitational response to imposed loads is small compared to their elastic response. In the analysis of such materials, special care must be taken to account properly for this response. In particular, methods employed to approximately account for the small elastic distortion of chain or wire rope under static mooring conditions can be inadequate in many conditions of physical interest, in particular when elasticity plays a dominant role. **Statmoor** incorporates an exact analytical expression for the combined elasto-gravitational static response of mooring line elements and thereby avoids altogether the problem of approximating the effects of either gravity or elasticity.\* Furthermore, the exact equations used in the code apply to arbitrary degrees of non-linearity in the elasticity of the elements, thereby rendering the analysis of highly non-linear synthetic elements completely straightforward.

### *Capabilities of Statmoor*

1. Up to twenty-four individual mooring lines can be accommodated (12 mooring lines on some microcomputer versions).
2. Each mooring line may consist of up to three independent sublines. Each subline can have specifiable mass characteristics and non-linear elastic characteristics (tension-strain relationship may include up to cubic terms).
3. A concentrated weight and/or line support buoy can be specified between appropriate sublines.
4. The ocean bottom may be uniformly sloping, or anchor depths may be independently specified.
5. Either fairlead pretensions or pretension line angles can be specified.
6. System and individual line characteristics (net restoring force, line tensions, suspended lengths, etc.) are output for horizontal offsets of any magnitude in any direction and for yaw offsets both clockwise and counterclockwise.
7. English or metric units may be specified.

It should be noted that all offsets are by the "Hand of God" meaning that the vessel is not allowed to respond in any degree of freedom to the development of mooring forces as the offset is made. The totality of force and moments acting on the vessel during the offset are, however, output.

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\* It is sometimes erroneously claimed that a closed-form analytical solution of the combined elasto-gravitational "catenary" problem does not exist. See, for example, reference 2.

### *Special Applications*

**Statmoor**'s power and flexibility make it useful for the analysis of virtually any problem in which elastic lines or cables play a central role. Some examples of recent non-conventional applications:

1. Tension-offset characteristics for composite rubber hoses of various types used in offshore production facilities.
2. Tension-offset characteristics for composite towlines.
3. Surge and yaw restoring characteristics and tendon tensions for tension leg platforms and guyed towers.
4. Restoring force characteristics for submerged tethered buoys and SALMs.

### *Program Access*

**Statmoor** is available on an unlimited-use basis on a user's own equipment through a standard license agreement with SeaSoft. The license agreement permits the user to utilize **Statmoor** for any purpose other than resale or transfer to a third party. **Statmoor** is presently available to run on many mini- and microcomputers. In addition, individual timesharing accounts can be established. Special arrangements to configure **Statmoor** to run on any computer system with a suitable Fortran 77 compiler can be made.

## **II. Discussion Of Elasticity In Mooring Systems**

The large and growing family of synthetic materials is gradually setting the scene for a revolution in the design of offshore mooring systems. Ropes of nylon, Kevlar, Dacron and Polypropylene have already proven themselves superior to steel ropes for many offshore applications and their future utilization in mooring systems has been anticipated by a steadily growing number of studies of synthetic-steel composite mooring lines, especially for deep water moorings. [Ref. 3-5]. The virtues of synthetics include unsurpassed corrosion and fatigue resistance, light weight, ease of handling, and high elastic compliance which greatly reduces the tension peaks arising from wave-frequency fairlead motions. The inevitability of increased utilization of synthetics in mooring systems requires that state of the art mooring analyses accurately incorporate the (generally non-linear) elastic response characteristics of mooring materials in addition to the classical gravitational response associated with mooring line catenary adjustments. Most mooring analysis codes in wide use today treat line elastic response in an approximate manner. This approximation becomes increasingly unsatisfactory as the relative effects of elastic response increases and that of gravitational response decreases. In extreme cases these approximations can lead to line tension estimation errors of more than 100 percent (see Section III). Even for conventional mooring systems comprised only of wire rope the commonly utilized approximations to the elastic response can result in line tension estimate errors of more than 30 percent. **Statmoor** is the only mooring analysis code known to us which uses an exact representation of the combined elasto-gravitational static mooring line equations, thereby permitting an accurate analysis of complicated mooring systems which contain highly compliant components. In addition, nonlinear stress-elongation characteristics have been accommodated in the analytical model forming the basis of **Statmoor** in order to permit analysis of systems containing highly non-linear elastic components.

### III. Technical Evaluation of Statmoor

During the development and check-out of **Statmoor** it was found that at least some mooring programs currently in wide use are notably deficient in the analysis of mooring systems for which elastic deformation of the mooring line plays a role comparable in importance to the adjustment of the line shape under the action of gravity (catenary adjustment). This section is intended to identify some of those mooring configurations for which significant errors arise when using commonly applied approximation methods. The following conditions, in particular, are subject to error in elastic modeling by many conventional mooring programs:

1. Systems in which light, elastic synthetic materials (Kevlar, nylon, polypropylene) are prominent elements in the mooring system. These include the family of composite lines which have in recent years received attention for deep water mooring systems. Computational errors for these systems can be substantial, in particular, under conditions of large pretension.
2. Systems in which very large clump weights and high pretensions are used to create a "stiff" mooring system for operational conditions which "soften" during large-excursion survival conditions. This would include, for example, guyed tower applications.

#### *Comparative Analysis*

To illustrate the magnitude of the errors which can develop, the output of **Statmoor**, Ultramarine's OSCAR and an early (1972) version of the Exxon CALMS program were compared (during fall 1982) in four systems:

System Description	Water Depth	Subline Composition	Line AE (lbs)*	Weight in Water (lbs/ft)	Lumped Weight (kips)
<b>Case 1:</b> Kevlar/Lumped Weight/Wire/Anchor Pretension 300 kips	1500'	2000'x4" Kevlar 1000'x3.5" Wire	1.20x10 <sup>7</sup> 8.65x10 <sup>7</sup>	1.01 17.10	280
<b>Case 2:</b> Kevlar/Pile Anchor Pretension 60 kips	4500'	6000'x4" Kevlar	4.00x10 <sup>7</sup>	1.01	N.A.
<b>Case 3:</b> Wire/Lumped Weight/Wire/Anchor Pretension 300 kips	1500'	2500'x3.5" Wire 1000'x3.5" Wire	8.65x10 <sup>7</sup> 8.65x10 <sup>7</sup>	17.10 17.10	280
<b>Case 4:</b> Kevlar/Chain/ Anchor Pretension 150 kips	3500'	6000'x4" Kevlar 500'x6" Chain	1.20x10 <sup>7</sup> 4.10x10 <sup>9</sup>	1.01 368.00	N.A.

\* The small AE values for Kevlar in these cases can be achieved by proper rope design.

Note that the systems described here are not intended to be optimized designs in any way. They have been selected only to illustrate the various general observations made above. All cases utilize a simple two-line moor (lines at 0° and 180°) with offsets towards one anchor. Case 1 represents a highly pretensioned, highly elastic system which might be a candidate concept for a future guyed tower design utilizing the excellent fatigue and corrosion properties of Kevlar in a circumstance where the possibility of chafing of the Kevlar elements would be minimal. The offset producing clump liftoff is a particularly sensitive function of the treatment of elasticity; for this simple system, **Statmoor**'s results can be demonstrated to be correct. (Figure 1)

Case 2 represents a mooring which might be considered for a deep water production platform. The restoring force characteristics are again very strongly dependent on the elastic properties; **Statmoor**'s results can be shown to be correct; see the following subsection. (Figure 2)

Case 3 represents a more-or-less conventional guyed-tower type moor with heavy wire rope members and a large clump weight. Because of the high pretensions used the elasticity of the wire rope is quite important, as indicated by differences in excess of 30% between the exact (**Statmoor**) treatment and the approximate treatments. (Figure 3)

Case 4 represents a typical Kevlar-chain composite system which has been proposed for deep water mooring systems. A particularly interesting feature of this example is the large overestimate of anchor uplift resulting from the errors in conventional modelling of the elastic behavior of the Kevlar. (Figure 4)

In summary, note should be made of the following:

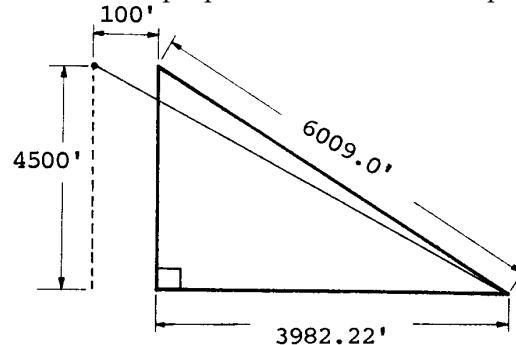
1. In highly tensioned deep water elastic systems, errors of 100% are possible (Figures 1, 2).
2. Although the largest errors are associated with light, highly elastic synthetic materials, the performance of wire rope can under special circumstances be significantly misjudged - see Figure 3, where the maximum errors amount to nearly 40%.

### *Validation of Statmoor Predictions*

**Statmoor**'s predictions have been checked by hand in a wide variety of limiting cases including the totally inelastic limit (catenary) and the totally elastic limit (neutrally buoyant lines). An example of one of these checks is outlined below for Case 2 (Figure 2) of this section.

For the large tensions associated with Case 2, Kevlar can be considered neutrally buoyant and the restoring force from a single line can be computed with high accuracy from purely geometrical considerations applied to the assumed linear elastic properties of the Kevlar rope:

- 1) Line length at zero tension 6000'
- 2) Line length at 60 kips pretension 6009.00'
- 3) Line length for 100' offset 6075.73'
- 4) Total tension for 100' offset 504.88 kips
- 5) Horizontal tension for 100' offset 339.23 kips



Note that the second (shortened) line of case #2 is slack for a 100' offset condition, so that the total restoring force associated with the 100' offset is approximately 339 kips. (Figure 2). The above geometrical technique has also been used to verify **Statmoor**'s prediction of clump weight liftoff in Case 1 (Figure 1). Here again **Statmoor** yields the exact solution.

## IV. Treatment of Bottom Friction

Traditionally bottom friction has been accommodated for in static mooring programs by the specification of a friction coefficient and incorporation of a simple tension correction calculation based on the assumption that the tension in each line under all conditions of offset has been reached by a uniform monotonic *increase* in tension from low values. This assumption is clearly fallacious since many of the mooring lines, for any offset condition other than zero, have a lower tension than they had at zero offset. Furthermore, under weakly dynamic conditions, the tension in each line will oscillate slightly about the mean. It is a consequence of the irreversibility, or hysteresis, inherent in all dissipative processes such as friction that the recent tension history for each individual line must be considered in the determination of its instantaneous state. A careful analysis of the consequences of bottom friction for the calculation of static offset restoring characteristics shows that the complete neglect of bottom friction will most realistically reproduce the average static offset characteristics one would measure in a weakly dynamic environment. This approach has been adopted in **Statmoor**. The physical basis for this procedure is best understood by considering the friction-associated hysteresis curve for a single line, as depicted in a schematically exaggerated way in Figure 5. As a fairlead undergoes even infinitesimal horizontal oscillations about a particular point, for instance its zero offset point, the line tension jumps discontinuously between the two hysteresis branches due to the action of elastic elongation in the presence of friction. Since every environment is at least weakly dynamic, it is clear that the most reasonable single value of tension for a given fairlead-anchor distance is given by the average of the double - valued tension function, which average is adequately represented by the curve representing the case of zero friction. It must be stressed that these comments apply to *static offsets only*. When considering quasi-static or fully dynamic conditions, the energy loss due to friction effects can play an important role and must be carefully accounted for.

## V. Description Of User Interface

The user interface, a flexible and easy-to-use input file editor, was created to provide a user-friendly question-and-answer environment for the preparation and editing of the input file required by **Statmoor**. The interface has been designed to permit the first-time user to execute **Statmoor** without studying the input file structure and format requirements or learning a specialized and easily forgotten nomenclature. A knowledge of computer programming is not required for utilization of **Statmoor**. The following special features of the user interface should be noted:

1. *Help* facility for effective weight/unit length and breaking strength of mooring lines: This provides approximate default values for breaking strengths and for effective weights of a wide variety of mooring materials in seawater, fresh water and air. Although variations in line properties between different manufacturers are generally small, it is recommended that manufacturer's data, when available, be used in lieu of default values. Reference 1 contains specific illustrations of the *Help* facility.
2. *Help* facility for elastic coefficients of mooring lines: This provides two types of help: (i) default values for a wide variety of mooring materials; and (ii) a curve-fitting routine to compute the required coefficients from manufacturer supplied curves or tables of elongation versus line tension. Note that the default values supplied by the *Help* facility for synthetic material, in particular nylon and Nystron, apply to wet, stabilized lines.

## VI. Input Description And Discussion

### *General*

Before **Statmoor** can be exercised, all relevant physical data for the mooring system to be analyzed must be gathered. When available, manufacturer's data for the specific materials to be used should be obtained.

The list of input parameters which should be prepared before attempting to execute **Statmoor** follow:

#### *A. General Layout*

1. Number of mooring lines.
2. Plan view layout of the lines with the fairlead-anchor direction for each. Every mooring line is assigned a unique number; the number serves to associate each line with its physical characteristics. Thus, the first fairlead-anchor direction to be specified is associated with Line Number 1, etc. Numbering should normally begin with the most forward line on the starboard side and progress in a counter-clockwise direction. See Figure 6 for a sample layout.
3. Spatial coordinates (x,y,z) of each fairlead. x (forward) and y (starboard) coordinates are required only if yaw restoring characteristics and pitch/roll moments are desired.
4. Depth of water beneath vessel.
5. Slope of ocean bottom, if uniform, or depth of each anchor.
6. Direction of maximum downwards slope (the "slope direction").

#### *B. Details of Mooring Lines*

1. Complete description of each type of mooring line to be used, including length, weight/unit length in water, nominal diameter and breaking strength of each subline component of a particular composite line. Each line can consist of at most three independent sublines. There are no restrictions on the composition of the sublines. A lumped weight or sinker can be specified between the two anchor-side sublines, and a mooring buoy can be specified between the fairlead-side sublines.

**Note:** Default weight/unit length values and breaking strengths for a wide variety of mooring materials including chain, IWRC wire rope, Kevlar and nylon are available through the "Help" facility of the user interface sub-program described in Section V.

2. Complete description of the elastic characteristics of each subline component of a particular composite line. For elements with approximately linear elasticity, such as chain and wire rope, the EA value for the specified line should be obtained. For elements with nonlinear elastic properties, manufacturer's data for the elastic component of elongation versus line tension should be obtained. The elastic component is that component which remains after all nonrecoverable elongation has been subtracted from the total elongation of new rope. Default values for the elastic coefficients of many mooring materials are available through the "Help" facility of the user interface. (See Section V.)
3. Submerged weight of any lumped weights or sinkers to be employed.
4. Submerged buoyancy of any mooring buoys to be employed.

*C. Zero-Offset (Pretension) Conditions*

1. Zero-offset line tensions at fairleads (total tension or horizontal component), declination angles at fairleads (measured from the horizontal), or fairlead-anchor horizontal separation.

*D. Offset Specifications*

1. Direction of each desired lateral offset sequence.
2. Actual lateral offset magnitudes from the zero-offset position. (Default offset increments are 1 percent of water depth).
3. Direction ("parity") of any desired yaw offset sequence. The possibilities are only two, clockwise and counter-clockwise.
4. Actual yaw offsets magnitudes from the zero-offset condition. (Default offset increments are 2.5 degrees).

*Miscellaneous Notes*

1. Dimensions: Either English or Metric units can be used in **Statmoor**. All lengths, depths, etc., should be input in feet (meters) *except* mooring line diameters, which should be input in inches (millimeters). All weights, forces or line tensions should be input in kips (metric tons) *except* line weights which should be input in pounds/feet (kilogram weight/meter).

**VII. Output Options**

The output stream from **Statmoor** consists of two distinct output types: mandatory and elective. The mandatory output includes:

- Tabular output of selected input parameters of importance.
- Tabular output of the zero-offset condition including distances to anchors, slope of bottom towards anchors, fairlead and anchor line tension components, and suspended line lengths.
- Tabular output of the physical characteristics of the most exposed (most highly loaded) line during each requested offset sequence.
- Tabular output of mooring system restoring characteristics for each requested offset sequence.

The elective output can be included or excluded as desired. The elective output includes, for every line and every specified offset condition:

- A cross-coupling summary which gives all forces and moments induced by the rigid transport of the vessel as specified in the offset requirements.
- Any or all tension components at the fairleads or anchors.
- Suspended line lengths.
- Declination angles at the fairleads.

## References

1. Program "Statmoor" Static Mooring Analysis Code: User's Manual, 1989. Available from SeaSoft Systems, 250 Ribera Drive, Suite B, Santa Barbara, CA 93111.
2. Fylling, I.J., "Anchor Line Forces" in the second WEGEMT (*West European Graduate Education Marine Technology*) Graduate School on Advanced Aspects of Offshore Engineering, The Norwegian Institute of Technology, January 1979, Vol. II.
3. A Study of the Comparative Mooring Performance of Kevlar and Steel Ropes, E. I. duPont de Nemours & Co. Report. Available through: Textile Fibers Department, Kevlar Marketing, Centre Road Building, Wilmington, Delaware 19898.
4. Pollack, J. and Hwang, Y., "A Permanent Mooring for a Deepwater Production System", 1982 Offshore Technology Proceedings, Paper # OTC 4347.
5. Niedzwecki, J. M., "A Comparison of Non-Metallic Ropes with Wire Rope and Chain Mooring Lines for Deep Water Applications", 1978 Offshore Technology Conference Proceedings, Paper #OTC 3207.
6. Finn, L. D., "A New Deepwater Offshore Platform - The Guyed Tower", 1976 Offshore Technology Conference Proceedings, Paper #OTC 2688.

## Sample Output

The following pages comprise a portion of the output from a **Statmoor** execution .

SeaSoft Systems Software Library

Volume 7  
Catenary Mooring Statics Calculator

Statmoor Version 4.60

Copyright (C) 1993  
By Richard J. Hartman, Ph.D.Statmoor Trial Run  
Deep Water Semi

Executed at 10:42 on 9/8/93

\*\*\*\*\* INTERPOLATION TABLES FOR LINE NUMBER 1 \*\*\*\*\*

INDEX	THTOP	TOPT	TZANC	THANC	XANC	SL
1	.078	4.801	.000	.078	2591.719	2001.845
2	7.483	8.890	.000	7.483	3765.668	2194.271
3	15.590	16.312	.000	15.590	3933.556	2374.312
4	24.464	24.930	.000	24.464	4020.668	2521.720
5	34.178	34.513	.000	34.178	4073.284	2605.083
6	44.812	45.068	.000	44.812	4109.604	2693.624
7	56.453	56.657	.000	56.453	4137.911	2785.780
8	69.196	69.363	.000	69.196	4161.581	2881.068
9	83.147	83.285	.000	83.147	4182.236	2979.449
10	98.418	98.535	.000	98.418	4200.779	3081.057
11	115.135	115.235	.000	115.135	4217.754	3186.110
12	133.436	133.522	.000	133.436	4233.521	3294.860
13	153.469	153.797	.000	153.469	4262.283	3368.846
14	175.399	176.141	.000	175.399	4286.140	3446.882
15	199.406	200.702	.000	199.406	4305.658	3531.607
16	225.686	227.661	.000	225.686	4322.051	3623.050
17	254.455	257.219	.000	254.455	4336.191	3721.294
18	285.948	289.598	.000	285.948	4348.714	3826.462
19	320.424	325.044	.000	320.424	4360.087	3938.712
20	358.164	363.829	.000	358.164	4370.659	4058.233
21	399.478	406.253	.000	399.478	4380.694	4185.240
22	444.703	452.646	.000	444.703	4390.398	4319.970
23	494.212	503.370	.000	494.212	4399.933	4462.680
24	548.409	558.847	9.009	548.409	4409.231	4500.000
25	607.738	619.581	22.064	607.738	4417.992	4500.000
26	672.685	686.069	36.357	672.685	4426.426	4500.000
27	743.782	758.854	51.996	743.782	4434.729	4500.000
28	821.611	838.531	69.098	821.611	4443.069	4500.000
29	906.811	925.748	87.789	906.811	4451.591	4500.000
30	1000.078	1021.217	108.208	1000.078	4460.429	4500.000

***** INTERPOLATION TABLES FOR LINE NUMBER 2 *****							***** MOORING LINE MASS CHARACTERISTICS SUMMARY *****							
INDEX	THTOP	TOPT	TZANC	THANC	XANC	SL	LINE NO.	-----	SUBLN INDEX	DATA LENGTH	NOMINAL COMP.	EFFECTIVE DIAMETER	SINKER WEIGHT	MOORING BUOY-NET
							(DEG)		(FT)	(IN)	(LBS/FT)	(K.LBS)		BUOANCY (K.LBS)
1	.078	.809	.000	.078	3222.459	1101.499								
2	7.483	9.019	.000	7.483	3743.198	2000.000								
3	15.590	18.310	.000	15.590	3758.530	2000.000								
4	24.464	28.455	.000	24.464	3773.233	2000.000								
5	34.178	39.525	.000	34.178	3788.385	2000.000								
6	44.812	51.601	.000	44.812	3804.081	2000.000								
7	56.453	64.776	.000	56.453	3820.292	2000.000								
8	69.196	79.151	.000	69.196	3836.951	2000.000								
9	83.147	94.839	.000	83.147	3853.962	2000.000								
10	98.418	111.963	.000	98.418	3871.202	2000.000								
11	115.135	130.659	.000	115.135	3888.525	2000.000								
12	133.436	151.076	.000	133.436	3905.758	2000.000								
13	153.469	173.382	.000	153.469	3922.701	2000.000								
14	175.399	197.759	.000	175.399	3939.135	2000.000								
15	199.406	224.406	.000	199.406	3954.859	2018.823								
16	225.686	253.230	.000	225.686	3971.869	2171.232								
17	254.455	284.301	.000	254.455	3990.173	2324.088								
18	285.948	317.910	.000	285.948	4008.569	2479.080								
19	320.424	354.355	.000	320.424	4026.393	2637.500								
20	358.164	393.944	.000	358.164	4043.373	2800.297								
21	399.478	437.002	.000	399.478	4059.601	2968.093								
22	444.703	483.867	.000	444.703	4075.573	3141.145								
23	494.212	534.900	.000	494.212	4092.306	3319.256								
24	548.409	590.479	.000	548.409	4111.517	3501.633								
25	607.738	651.001	.000	607.738	4135.879	3686.686								
26	672.685	716.886	.000	672.685	4169.375	3871.758								
27	743.782	788.584	4.157	743.782	4217.758	4000.000								
28	821.611	866.686	18.001	821.611	4288.803	4000.000								
29	906.811	951.660	30.844	906.811	4394.146	4000.000								
30	1000.078	1043.945	41.578	1000.078	4549.715	4000.000								

***** MOORING LINE ELASTIC CHARACTERISTICS SUMMARY *****										***** FAIRLEAD SUMMARY *****				
LINE NO.	HEADING (DEG)	SUBLINE DATA			ELASTIC COEFFICIENTS			FAIRLEAD NUMBER	LINE DIRECTION (DEG)	FAIRLEAD COORDINATES (FROM WATERLINE)				
		INDEX	LENGTH	COMP.	ALPHA1 (K.LBS**-1)	ALPHA2 (K.LBS**-2)	ALPHA3 (K.LBS**-3)			X (FT)	Y (FT)	Z (FT)		
1	.0	SUBLN 3	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 2	1500.0	Chain	0.220E-04	0.000E+00	0.000E+00							
		SUBLN 1	1000.0	Wire	0.230E-04	0.000E+00	0.000E+00							
2	90.0	SUBLN 2	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 1	2000.0	Nylon	0.667E-03	-0.126E-05	0.884E-09							
3	90.0	SUBLN 2	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 1	2000.0	Nylon	0.667E-03	-0.126E-05	0.884E-09							
4	180.0	SUBLN 3	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 2	1500.0	Chain	0.220E-04	0.000E+00	0.000E+00							
		SUBLN 1	1000.0	Wire	0.230E-04	0.000E+00	0.000E+00							
5	180.0	SUBLN 3	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 2	1500.0	Chain	0.220E-04	0.000E+00	0.000E+00							
		SUBLN 1	1000.0	Wire	0.230E-04	0.000E+00	0.000E+00							
6	270.0	SUBLN 2	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 1	2000.0	Nylon	0.667E-03	-0.126E-05	0.884E-09							
7	270.0	SUBLN 2	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 1	2000.0	Nylon	0.667E-03	-0.126E-05	0.884E-09							
8	360.0	SUBLN 3	2000.0	Chain	0.980E-05	0.000E+00	0.000E+00			150.00	150.00	.00		
		SUBLN 2	1500.0	Chain	0.220E-04	0.000E+00	0.000E+00							
		SUBLN 1	1000.0	Wire	0.230E-04	0.000E+00	0.000E+00							

***** ZERO-OFFSET CONDITION SUMMARY *****								***** OCEAN BOTTOM SUMMARY *****			
LINE NO.	ANCHOR- TO-FRLD HEIGHT (FT)	MEAN SLOPE TO ANCHOR (FT/FT)	FAIRLEAD- ANCHOR DISTANCE (FT)	UNSTRETCHED SUSPENDED LENGTH (FT)	ZERO-OFFSET FAIRLEAD TENSIONS --- LINE			BOTTOM:  DEPTH AT VESSEL 1000.00 FT BOTTOM SLOPE .000 FT/FT SLOPE DIRECTION .0 DEGREES FRICTION COEFFICIENT .000			
					TOTAL (K.LBS)	HORIZ. (K.LBS)	VERT. (K.LBS)				
1	1000.0	.000	4177.7	2957.8	80.00	79.85	-4.81	3.5			
2	1000.0	.000	3837.9	2000.0	80.00	69.95	-38.82	29.0			
3	1000.0	.000	3837.9	2000.0	80.00	69.95	-38.82	29.0			
4	1000.0	.000	4177.7	2957.8	80.00	79.85	-4.81	3.5			
5	1000.0	.000	4177.7	2957.8	80.00	79.85	-4.81	3.5			
6	1000.0	.000	3837.9	2000.0	80.00	69.95	-38.82	29.0			
7	1000.0	.000	3837.9	2000.0	80.00	69.95	-38.82	29.0			
8	1000.0	.000	4177.7	2957.8	80.00	79.85	-4.81	3.5			

***** LATERAL OFFSET RESTORING CHARACTERISTICS *****							***** LATERAL OFFSET RESTORING CHARACTERISTICS *****													
OFFSET DIRECTION = .00 DEG							OFFSET DIRECTION = .00 DEG													
---- MOST EXPOSED LINE CHARACTERISTICS ----																				
----- FAIRLEAD TENSIONS -----																				
OFFSET (FT)	LINE NO.	TOTAL (K.LBS)	HORIZ. (K.LBS)	VERT. (K.LBS)	LENGTH (FT)	UNSTRETCHED SUSPENDED (FT)	ANCHOR FORCES REL. TO BOTTOM (K.LBS)	PARALLEL (K.LBS)	PERP. (K.LBS)	RESTORING FORCE (K.LBS)										
.0	8	80.00	79.85	-4.81	2957.8	79.85	.00			.00										
10.0	5	87.76	87.63	-4.81	3009.3	87.63	.00			-29.36										
20.0	5	95.99	95.87	-4.81	3064.1	95.87	.00			-59.00										
30.0	5	105.33	105.22	-4.81	3123.8	105.22	.00			-89.20										
40.0	5	115.17	115.07	-4.80	3185.7	115.07	.00			-120.34										
50.0	5	126.75	126.66	-4.81	3254.6	126.66	.00			-152.49										
60.0	5	136.46	136.33	-5.75	3305.6	136.33	.00			-180.80										
70.0	5	143.51	143.30	-7.68	3331.3	143.30	.00			-203.24										
80.0	5	150.55	150.26	-9.33	3357.0	150.26	.00			-223.78										
90.0	5	158.85	158.43	-11.57	3386.5	158.43	.00			-246.72										
100.0	5	168.22	167.63	-14.14	3419.2	167.63	.00			-271.72										
110.0	5	178.08	177.30	-16.71	3453.6	177.30	.00			-296.47										
120.0	5	190.67	189.60	-20.17	3497.0	189.60	.00			-325.54										
130.0	5	204.03	202.65	-23.69	3542.9	202.65	.00			-356.12										
140.0	5	220.48	218.68	-28.07	3598.7	218.68	.00			-392.67										
150.0	5	239.43	237.15	-33.03	3662.2	237.15	.00			-434.08										
160.0	5	261.08	258.21	-38.60	3733.8	258.21	.00			-480.21										
170.0	5	286.93	283.36	-45.16	3817.8	283.36	.00			-533.36										
180.0	5	317.55	313.14	-52.77	3915.0	313.14	.00			-595.79										
190.0	5	352.91	347.54	-61.34	4024.6	347.54	.00			-667.48										
200.0	5	393.52	387.08	-70.91	4147.1	387.08	.00			-749.45										
210.0	5	439.67	432.05	-81.48	4282.3	432.05	.00			-842.29										
220.0	5	491.40	482.53	-92.95	4429.0	482.53	.00			-946.16										
230.0	5	549.61	539.39	-105.52	4500.0	539.39	.00			-1062.81										
240.0	5	617.44	605.64	-120.10	4500.0	605.64	21.60			-1198.27										

TOTAL RESTORING CHARACTERISTICS AND CROSS-COUPLING SUMMARY						
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OFFSET (FT)	TOTAL RESTORING FORCE (K.LBS)	ROLL ----- (K.LBS*FT)	INDUCED MOMENTS (ABOUT WATERLINE) ----- (K.LBS*FT)	PITCH ----- (K.LBS*FT)	YAW ----- (K.LBS*FT)	INDUCED FORCES ----- (K.LBS)
.0	.00	.00E+00	0.00E+00	0.00E+00	.00	.00
10.0	-29.36	0.00E+00	0.00E+00	0.00E+00	.00	-29.36
20.0	-59.00	0.00E+00	0.12E+01	0.00E+00	.00	-59.00
30.0	-89.20	0.00E+00	0.30E+01	0.00E+00	.00	-89.20
40.0	-120.34	0.00E+00	0.00E+00	0.00E+00	.00	-120.34
50.0	-152.49	0.00E+00	0.52E+01	0.00E+00	.00	-152.49
60.0	-180.80	0.00E+00	-0.28E+03	0.00E+00	.00	-180.80
70.0	-203.24	0.00E+00	-0.86E+03	0.00E+00	.00	-203.24
80.0	-223.78	0.00E+00	-0.13E+04	0.00E+00	.00	-223.78
90.0	-246.72	0.00E+00	-0.20E+04	0.00E+00	.00	-246.72
100.0	-271.72	0.00E+00	-0.28E+04	0.00E+00	.00	-271.72
110.0	-296.47	0.00E+00	-0.36E+04	0.00E+00	.00	-296.47
120.0	-325.54	0.00E+00	-0.46E+04	0.00E+00	.00	-325.54
130.0	-356.12	0.00E+00	-0.56E+04	0.00E+00	.00	-356.12
140.0	-392.67	0.00E+00	-0.70E+04	0.00E+00	.00	-392.67
150.0	-434.08	0.00E+00	-0.85E+04	0.00E+00	.00	-434.08
160.0	-480.21	0.00E+00	-0.10E+05	0.00E+00	.00	-480.21
170.0	-533.36	0.00E+00	-0.12E+05	0.00E+00	.00	-533.36
180.0	-595.79	0.00E+00	-0.14E+05	0.00E+00	.00	-595.79
190.0	-667.48	0.00E+00	-0.17E+05	0.00E+00	.00	-667.48
200.0	-749.45	0.00E+00	-0.20E+05	0.00E+00	.00	-749.45
210.0	-842.29	0.00E+00	-0.23E+05	0.00E+00	.00	-842.29
220.0	-946.16	0.00E+00	-0.26E+05	0.00E+00	.00	-946.16
230.0	-1062.81	0.00E+00	-0.30E+05	0.00E+00	.00	-1062.81
240.0	-1198.27	0.00E+00	-0.35E+05	0.00E+00	.00	-1198.27

***** TOTAL FAIRLEAD LINE TENSION (K.LBS)									***** HORIZONTAL TENSION COMPONENTS (K.LBS)								
***** OFFSET DIRECTION = .00 DEG									***** OFFSET DIRECTION = .00 DEG								
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )									OFFSET (FT )								
.00	80.00	80.00	80.00	80.00	80.00	80.00	80.00	80.00	.00	79.85	69.95	69.95	79.85	79.85	69.95	69.95	79.85
10.00	73.48	80.04	80.04	87.76	87.76	80.04	80.04	73.48	10.00	73.32	69.99	69.99	87.63	87.63	69.99	69.99	73.32
20.00	67.27	80.08	80.08	95.99	95.99	80.08	80.08	67.27	20.00	67.10	70.02	70.02	95.87	95.87	70.02	70.02	67.10
30.00	61.90	80.14	80.14	105.33	105.33	80.14	80.14	61.90	30.00	61.71	70.07	70.07	105.22	105.22	70.07	70.07	61.71
40.00	56.56	80.22	80.22	115.17	115.17	80.22	80.22	56.56	40.00	56.36	70.15	70.15	115.07	115.07	70.15	70.15	56.36
50.00	52.47	80.33	80.33	126.75	126.75	80.33	80.33	52.47	50.00	52.25	70.24	70.24	126.66	126.66	70.24	70.24	52.25
60.00	48.38	80.46	80.46	136.46	136.46	80.46	80.46	48.38	60.00	48.13	70.36	70.36	136.33	136.33	70.36	70.36	48.13
70.00	44.51	80.62	80.62	143.51	143.51	80.62	80.62	44.51	70.00	44.25	70.50	70.50	143.30	143.30	70.50	70.50	44.25
80.00	41.60	80.80	80.80	150.55	150.55	80.80	80.80	41.60	80.00	41.32	70.66	70.66	150.26	150.26	70.66	70.66	41.32
90.00	38.70	81.00	81.00	158.85	158.85	81.00	81.00	38.70	90.00	38.39	70.84	70.84	158.43	158.43	70.84	70.84	38.39
100.00	35.79	81.23	81.23	168.22	168.22	81.23	81.23	35.79	100.00	35.47	71.04	71.04	167.63	167.63	71.04	71.04	35.47
110.00	33.49	81.48	81.48	178.08	178.08	81.48	81.48	33.49	110.00	33.14	71.27	71.27	177.30	177.30	71.27	71.27	33.14
120.00	31.67	81.76	81.76	190.67	190.67	81.76	81.76	31.67	120.00	31.30	71.51	71.51	189.60	189.60	71.51	71.51	31.30
130.00	29.85	82.06	82.06	204.03	204.03	82.06	82.06	29.85	130.00	29.45	71.78	71.78	202.65	202.65	71.78	71.78	29.45
140.00	28.03	82.38	82.38	220.48	220.48	82.38	82.38	28.03	140.00	27.60	72.07	72.07	218.68	218.68	72.07	72.07	27.60
150.00	26.21	82.73	82.73	239.43	239.43	82.73	82.73	26.21	150.00	25.76	72.38	72.38	237.15	237.15	72.38	72.38	25.76
160.00	24.63	83.10	83.10	261.08	261.08	83.10	83.10	24.63	160.00	24.16	72.71	72.71	258.21	258.21	72.71	72.71	24.16
170.00	23.65	83.50	83.50	286.93	286.93	83.50	83.50	23.65	170.00	23.14	73.06	73.06	283.36	283.36	73.06	73.06	23.14
180.00	22.66	83.92	83.92	317.55	317.55	83.92	83.92	22.66	180.00	22.12	73.44	73.44	313.14	313.14	73.44	73.44	22.12
190.00	21.67	84.36	84.36	352.91	352.91	84.36	84.36	21.67	190.00	21.10	73.83	73.83	347.54	347.54	73.83	73.83	21.10
200.00	20.68	84.83	84.83	393.52	393.52	84.83	84.83	20.68	200.00	20.08	74.25	74.25	387.08	387.08	74.25	74.25	20.08
210.00	19.69	85.32	85.32	439.67	439.67	85.32	85.32	19.69	210.00	19.07	74.68	74.68	432.05	432.05	74.68	74.68	19.07
220.00	18.70	85.84	85.84	491.40	491.40	85.84	85.84	18.70	220.00	18.05	75.14	75.14	482.53	482.53	75.14	75.14	18.05
230.00	17.71	86.38	86.38	549.61	549.61	86.38	86.38	17.71	230.00	17.03	75.62	75.62	539.39	539.39	75.62	75.62	17.03
240.00	16.72	86.94	86.94	617.44	617.44	86.94	86.94	16.72	240.00	16.01	76.12	76.12	605.64	605.64	76.12	76.12	16.01

***** VERTICAL TENSION COMPONENTS (K.LBS) *****									***** ANCHOR PULL PERPENDICULAR TO BOTTOM (K.LBS) *****								
OFFSET DIRECTION = .00 DEG									OFFSET DIRECTION = .00 DEG								
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )									OFFSET (FT )								
.00	-4.81	-38.82	-38.82	-4.81	-4.81	-38.82	-38.82	-4.81	.00	.00	.00	.00	.00	.00	.00	.00	.00
10.00	-4.82	-38.84	-38.84	-4.81	-4.81	-38.84	-38.84	-4.82	10.00	.00	.00	.00	.00	.00	.00	.00	.00
20.00	-4.81	-38.85	-38.85	-4.81	-4.81	-38.85	-38.85	-4.81	20.00	.00	.00	.00	.00	.00	.00	.00	.00
30.00	-4.82	-38.88	-38.88	-4.81	-4.81	-38.88	-38.88	-4.82	30.00	.00	.00	.00	.00	.00	.00	.00	.00
40.00	-4.80	-38.92	-38.92	-4.80	-4.80	-38.92	-38.92	-4.80	40.00	.00	.00	.00	.00	.00	.00	.00	.00
50.00	-4.83	-38.97	-38.97	-4.81	-4.81	-38.97	-38.97	-4.83	50.00	.00	.00	.00	.00	.00	.00	.00	.00
60.00	-4.83	-39.03	-39.03	-5.75	-5.75	-39.03	-39.03	-4.83	60.00	.00	.00	.00	.00	.00	.00	.00	.00
70.00	-4.81	-39.10	-39.10	-7.68	-7.68	-39.10	-39.10	-4.81	70.00	.00	.00	.00	.00	.00	.00	.00	.00
80.00	-4.84	-39.18	-39.18	-9.33	-9.33	-39.18	-39.18	-4.84	80.00	.00	.00	.00	.00	.00	.00	.00	.00
90.00	-4.84	-39.28	-39.28	-11.57	-11.57	-39.28	-39.28	-4.84	90.00	.00	.00	.00	.00	.00	.00	.00	.00
100.00	-4.82	-39.38	-39.38	-14.14	-14.14	-39.38	-39.38	-4.82	100.00	.00	.00	.00	.00	.00	.00	.00	.00
110.00	-4.82	-39.50	-39.50	-16.71	-16.71	-39.50	-39.50	-4.82	110.00	.00	.00	.00	.00	.00	.00	.00	.00
120.00	-4.85	-39.62	-39.62	-20.17	-20.17	-39.62	-39.62	-4.85	120.00	.00	.00	.00	.00	.00	.00	.00	.00
130.00	-4.87	-39.76	-39.76	-23.69	-23.69	-39.76	-39.76	-4.87	130.00	.00	.00	.00	.00	.00	.00	.00	.00
140.00	-4.86	-39.91	-39.91	-28.07	-28.07	-39.91	-39.91	-4.86	140.00	.00	.00	.00	.00	.00	.00	.00	.00
150.00	-4.83	-40.07	-40.07	-33.03	-33.03	-40.07	-40.07	-4.83	150.00	.00	.00	.00	.00	.00	.00	.00	.00
160.00	-4.82	-40.24	-40.24	-38.60	-38.60	-40.24	-40.24	-4.82	160.00	.00	.00	.00	.00	.00	.00	.00	.00
170.00	-4.86	-40.42	-40.42	-45.16	-45.16	-40.42	-40.42	-4.86	170.00	.00	.00	.00	.00	.00	.00	.00	.00
180.00	-4.89	-40.61	-40.61	-52.77	-52.77	-40.61	-40.61	-4.89	180.00	.00	.00	.00	.00	.00	.00	.00	.00
190.00	-4.91	-40.82	-40.82	-61.34	-61.34	-40.82	-40.82	-4.91	190.00	.00	.00	.00	.00	.00	.00	.00	.00
200.00	-4.92	-41.03	-41.03	-70.91	-70.91	-41.03	-41.03	-4.92	200.00	.00	.00	.00	.00	.00	.00	.00	.00
210.00	-4.91	-41.26	-41.26	-81.48	-81.48	-41.26	-41.26	-4.91	210.00	.00	.00	.00	.00	.00	.00	.00	.00
220.00	-4.89	-41.49	-41.49	-92.95	-92.95	-41.49	-41.49	-4.89	220.00	.00	.00	.00	.00	.00	.00	.00	.00
230.00	-4.86	-41.74	-41.74	-105.52	-105.52	-41.74	-41.74	-4.86	230.00	.00	.00	.00	.00	.00	.00	.00	.00
240.00	-4.82	-42.00	-42.00	-120.10	-120.10	-42.00	-42.00	-4.82	240.00	.00	.00	.00	.00	.00	.00	.00	.00

***** SUSPENDED LINE LENGTHS (FT) *****									***** DECLINATION ANGLES AT FAIRLEAD (DEG) *****								
***** OFFSET DIRECTION = .00 DEG									***** OFFSET DIRECTION = .00 DEG								
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )									OFFSET (FT )								
.00	2957.76	2000.00	2000.00	2957.76	2957.76	2000.00	2000.00	2957.76	.00	3.45	29.03	29.03	3.45	3.45	29.03	29.03	3.45
10.00	2910.13	2000.00	2000.00	3009.30	3009.30	2000.00	2000.00	2910.13	10.00	3.76	29.03	29.03	3.14	3.14	29.03	29.03	3.76
20.00	2865.38	2000.00	2000.00	3064.09	3064.09	2000.00	2000.00	2865.38	20.00	4.10	29.03	29.03	2.87	2.87	29.03	29.03	4.10
30.00	2825.12	2000.00	2000.00	3123.79	3123.79	2000.00	2000.00	2825.12	30.00	4.47	29.02	29.02	2.62	2.62	29.02	29.02	4.47
40.00	2785.04	2000.00	2000.00	3185.67	3185.67	2000.00	2000.00	2785.04	40.00	4.87	29.02	29.02	2.39	2.39	29.02	29.02	4.87
50.00	2752.48	2000.00	2000.00	3254.59	3254.59	2000.00	2000.00	2752.48	50.00	5.28	29.02	29.02	2.18	2.18	29.02	29.02	5.28
60.00	2719.93	2000.00	2000.00	3305.57	3305.57	2000.00	2000.00	2719.93	60.00	5.73	29.02	29.02	2.42	2.42	29.02	29.02	5.73
70.00	2688.94	2000.00	2000.00	3331.29	3331.29	2000.00	2000.00	2688.94	70.00	6.20	29.01	29.01	3.07	3.07	29.01	29.01	6.20
80.00	2664.56	2000.00	2000.00	3357.01	3357.01	2000.00	2000.00	2664.56	80.00	6.68	29.01	29.01	3.55	3.55	29.01	29.01	6.68
90.00	2640.18	2000.00	2000.00	3386.51	3386.51	2000.00	2000.00	2640.18	90.00	7.19	29.01	29.01	4.18	4.18	29.01	29.01	7.19
100.00	2615.81	2000.00	2000.00	3419.22	3419.22	2000.00	2000.00	2615.81	100.00	7.74	29.00	29.00	4.82	4.82	29.00	29.00	7.74
110.00	2596.21	2000.00	2000.00	3453.58	3453.58	2000.00	2000.00	2596.21	110.00	8.28	29.00	29.00	5.38	5.38	29.00	29.00	8.28
120.00	2580.37	2000.00	2000.00	3496.99	3496.99	2000.00	2000.00	2580.37	120.00	8.82	28.99	28.99	6.07	6.07	28.99	28.99	8.82
130.00	2564.52	2000.00	2000.00	3542.90	3542.90	2000.00	2000.00	2564.52	130.00	9.38	28.98	28.98	6.67	6.67	28.98	28.98	9.38
140.00	2548.68	2000.00	2000.00	3598.69	3598.69	2000.00	2000.00	2548.68	140.00	9.98	28.98	28.98	7.31	7.31	28.98	28.98	9.98
150.00	2532.83	2000.00	2000.00	3662.18	3662.18	2000.00	2000.00	2532.83	150.00	10.62	28.97	28.97	7.93	7.93	28.97	28.97	10.62
160.00	2516.67	2000.00	2000.00	3733.83	3733.83	2000.00	2000.00	2516.67	160.00	11.27	28.96	28.96	8.50	8.50	28.96	28.96	11.27
170.00	2499.75	2000.00	2000.00	3817.81	3817.81	2000.00	2000.00	2499.75	170.00	11.86	28.95	28.95	9.06	9.06	28.95	28.95	11.86
180.00	2482.83	2000.00	2000.00	3914.99	3914.99	2000.00	2000.00	2482.83	180.00	12.46	28.95	28.95	9.57	9.57	28.95	28.95	12.46
190.00	2465.90	2000.00	2000.00	4024.59	4024.59	2000.00	2000.00	2465.90	190.00	13.09	28.94	28.94	10.01	10.01	28.94	28.94	13.09
200.00	2448.98	2000.00	2000.00	4147.14	4147.14	2000.00	2000.00	2448.98	200.00	13.75	28.93	28.93	10.38	10.38	28.93	28.93	13.75
210.00	2432.06	2000.00	2000.00	4282.27	4282.27	2000.00	2000.00	2432.06	210.00	14.44	28.92	28.92	10.68	10.68	28.92	28.92	14.44
220.00	2415.14	2000.00	2000.00	4429.00	4429.00	2000.00	2000.00	2415.14	220.00	15.17	28.91	28.91	10.90	10.90	28.91	28.91	15.17
230.00	2398.22	2000.00	2000.00	4500.00	4500.00	2000.00	2000.00	2398.22	230.00	15.94	28.90	28.90	11.07	11.07	28.90	28.90	15.94
240.00	2381.30	2000.00	2000.00	4500.00	4500.00	2000.00	2000.00	2381.30	240.00	16.76	28.89	28.89	11.22	11.22	28.89	28.89	16.76

***** LATERAL OFFSET RESTORING CHARACTERISTICS *****							***** LATERAL OFFSET RESTORING CHARACTERISTICS *****						
UNSTRETCHED ANCHOR FORCES TOTAL							TOTAL RESTORING CHARACTERISTICS AND CROSS-COUPLING SUMMARY						
OFFSET (FT)	LINE NO.	-- FAIRLEAD TENSIONS --		SUSPENDED LENGTH (FT)	ANCHOR FORCES REL. TO BOTTOM (K.LBS)	TOTAL RESTORING FORCE (K.LBS)	INDUCED MOMENTS (ABOUT WATERLINE) INDUCED FORCES						
		TOTAL HORIZ. VERT. (K.LBS) (K.LBS)					TOTAL RESTORING FORCE ROLL PITCH YAW TO OFFSET SURGE SWAY HEAVE						
.0	8	80.00	79.85	-4.81	2957.8	79.85	.00	.00	.00	.00	.00	.00	-174.53
10.0	7	89.25	78.18	-43.06	2000.0	78.18	.00	-32.57	10.0	-32.57	0.25E+04	0.00E+00	0.00E+00
20.0	7	98.75	86.64	-47.39	2000.0	86.64	.00	-65.33	20.0	-65.33	0.50E+04	0.00E+00	0.00E+00
30.0	7	108.68	95.49	-51.90	2000.0	95.49	.00	-98.18	30.0	-98.18	0.75E+04	0.00E+00	0.00E+00
40.0	7	119.19	104.88	-56.63	2000.0	104.88	.00	-131.59	40.0	-131.59	0.10E+05	0.00E+00	0.00E+00
50.0	7	129.99	114.53	-61.47	2000.0	114.53	.00	-165.17	50.0	-165.17	0.13E+05	0.00E+00	0.00E+00
60.0	7	141.77	125.09	-66.71	2000.0	125.09	.00	-199.89	60.0	-199.89	0.15E+05	0.00E+00	0.00E+00
70.0	7	153.90	135.97	-72.09	2000.0	135.97	.00	-234.84	70.0	-234.84	0.18E+05	0.00E+00	0.00E+00
80.0	7	167.06	147.79	-77.89	2000.0	147.79	.00	-271.25	80.0	-271.25	0.21E+05	0.00E+00	0.00E+00
90.0	7	181.10	160.41	-84.05	2000.0	160.41	.00	-307.83	90.0	-307.83	0.23E+05	0.00E+00	0.00E+00
100.0	7	195.93	173.75	-90.54	2000.0	173.75	.00	-340.43	100.0	-340.43	0.26E+05	0.00E+00	0.00E+00
110.0	7	212.62	188.78	-97.81	2010.5	188.78	.00	-371.57	110.0	-371.57	0.28E+05	0.00E+00	0.00E+00
120.0	7	229.56	204.11	-105.07	2046.1	204.11	.00	-403.30	120.0	-403.30	0.30E+05	0.00E+00	0.00E+00
130.0	7	246.51	219.56	-112.07	2135.7	219.56	.00	-435.28	130.0	-435.28	0.32E+05	0.00E+00	0.00E+00
140.0	7	263.47	235.17	-118.80	2221.6	235.17	.00	-467.60	140.0	-467.60	0.35E+05	0.00E+00	0.00E+00
150.0	7	280.49	250.89	-125.32	2305.1	250.89	.00	-500.13	150.0	-500.13	0.38E+05	0.00E+00	0.00E+00
160.0	7	298.42	267.69	-131.91	2389.2	267.69	.00	-534.84	160.0	-534.84	0.40E+05	0.00E+00	0.00E+00
170.0	7	316.69	284.81	-138.49	2473.5	284.81	.00	-570.19	170.0	-570.19	0.42E+05	0.00E+00	0.00E+00
180.0	7	336.99	304.00	-145.42	2562.0	304.00	.00	-609.70	180.0	-609.70	0.45E+05	0.00E+00	0.00E+00
190.0	7	357.87	323.78	-152.45	2652.0	323.78	.00	-650.38	190.0	-650.38	0.48E+05	0.00E+00	0.00E+00
200.0	7	381.19	346.00	-159.96	2747.8	346.00	.00	-695.97	200.0	-695.97	0.52E+05	0.00E+00	0.00E+00
210.0	7	405.96	369.69	-167.72	2847.1	369.69	.00	-744.51	210.0	-744.51	0.56E+05	0.00E+00	0.00E+00
220.0	7	432.49	395.15	-175.80	2950.5	395.15	.00	-796.60	220.0	-796.60	0.60E+05	0.00E+00	0.00E+00
230.0	7	461.36	422.98	-184.22	3058.0	422.98	.00	-853.44	230.0	-853.44	0.64E+05	0.00E+00	0.00E+00
240.0	7	490.97	451.59	-192.65	3165.9	451.59	.00	-911.87	240.0	-911.87	0.68E+05	0.00E+00	0.00E+00

***** TOTAL FAIRLEAD LINE TENSION (K.LBS) *****								***** HORIZONTAL TENSION COMPONENTS (K.LBS) *****									
OFFSET DIRECTION = 90.00 DEG								OFFSET DIRECTION = 90.00 DEG									
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )									OFFSET (FT )								
.00	80.00	80.00	80.00	80.00	80.00	80.00	80.00	80.00	.00	79.85	69.95	69.95	79.85	79.85	69.95	69.95	79.85
10.00	80.22	71.34	71.34	80.22	80.22	89.25	89.25	80.22	10.00	80.08	62.27	62.27	80.08	80.08	78.18	78.18	80.08
20.00	80.25	62.83	62.83	80.25	80.25	98.75	98.75	80.25	20.00	80.10	54.74	54.74	80.10	80.10	86.64	86.64	80.10
30.00	80.29	54.71	54.71	80.29	80.29	108.68	108.68	80.29	30.00	80.14	47.56	47.56	80.14	80.14	95.49	95.49	80.14
40.00	80.35	46.85	46.85	80.35	80.35	119.19	119.19	80.35	40.00	80.20	40.63	40.63	80.20	80.20	104.88	104.88	80.20
50.00	80.42	39.17	39.17	80.42	80.42	129.99	129.99	80.42	50.00	80.27	33.87	33.87	80.27	80.27	114.53	114.53	80.27
60.00	80.51	31.87	31.87	80.51	80.51	141.77	141.77	80.51	60.00	80.36	27.46	27.46	80.36	80.36	125.09	125.09	80.36
70.00	80.61	24.78	24.78	80.61	80.61	153.90	153.90	80.61	70.00	80.47	21.25	21.25	80.47	80.47	135.97	135.97	80.47
80.00	80.73	17.93	17.93	80.73	80.73	167.06	167.06	80.73	80.00	80.59	15.26	15.26	80.59	80.59	147.79	147.79	80.59
90.00	80.87	11.87	11.87	80.87	80.87	181.10	181.10	80.87	90.00	80.73	9.97	9.97	80.73	80.73	160.41	160.41	80.73
100.00	81.02	8.94	8.94	81.02	81.02	195.93	195.93	81.02	100.00	80.88	7.41	7.41	80.88	80.88	173.75	173.75	80.88
110.00	81.19	8.78	8.78	81.19	81.19	212.62	212.62	81.19	110.00	81.05	7.27	7.27	81.05	81.05	188.78	188.78	81.05
120.00	81.38	8.62	8.62	81.38	81.38	229.56	229.56	81.38	120.00	81.24	7.12	7.12	81.24	81.24	204.11	204.11	81.24
130.00	81.58	8.46	8.46	81.58	81.58	246.51	246.51	81.58	130.00	81.44	6.98	6.98	81.44	81.44	219.56	219.56	81.44
140.00	81.80	8.30	8.30	81.80	81.80	263.47	263.47	81.80	140.00	81.66	6.84	6.84	81.66	81.66	235.17	235.17	81.66
150.00	82.03	8.15	8.15	82.03	82.03	280.45	280.45	82.03	150.00	81.89	6.70	6.70	81.89	81.89	250.89	250.89	81.89
160.00	82.28	7.99	7.99	82.28	82.28	298.42	298.42	82.28	160.00	82.14	6.55	6.55	82.14	82.14	267.69	267.69	82.14
170.00	82.55	7.83	7.83	82.55	82.55	316.69	316.69	82.55	170.00	82.41	6.41	6.41	82.41	82.41	284.81	284.81	82.41
180.00	82.83	7.67	7.67	82.83	82.83	336.99	336.99	82.83	180.00	82.69	6.27	6.27	82.69	82.69	304.00	304.00	82.69
190.00	83.13	7.52	7.52	83.13	83.13	357.87	357.87	83.13	190.00	82.99	6.13	6.13	82.99	82.99	323.78	323.78	82.99
200.00	83.48	7.36	7.36	83.48	83.48	381.19	381.19	83.48	200.00	83.34	5.99	5.99	83.34	83.34	346.00	346.00	83.34
210.00	83.88	7.20	7.20	83.88	83.88	405.96	405.96	83.88	210.00	83.74	5.84	5.84	83.74	83.74	369.69	369.69	83.74
220.00	84.30	7.04	7.04	84.30	84.30	432.49	432.49	84.30	220.00	84.16	5.70	5.70	84.16	84.16	395.15	395.15	84.16
230.00	84.74	6.89	6.89	84.74	84.74	461.36	461.36	84.74	230.00	84.61	5.56	5.56	84.61	84.61	422.98	422.98	84.61
240.00	85.21	6.73	6.73	85.21	85.21	490.97	490.97	85.21	240.00	85.07	5.42	5.42	85.07	85.07	451.59	451.59	85.07

***** VERTICAL TENSION COMPONENTS (K.LBS) *****									***** ANCHOR PULL PERPENDICULAR TO BOTTOM (K.LBS) *****								
OFFSET DIRECTION = 90.00 DEG									OFFSET DIRECTION = 90.00 DEG								
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )									OFFSET (FT )								
.00	-4.81	-38.82	-38.82	-4.81	-4.81	-38.82	-38.82	-4.81	.00	.00	.00	.00	.00	.00	.00	.00	.00
10.00	-4.81	-34.81	-34.81	-4.81	-4.81	-43.06	-43.06	-4.81	10.00	.00	.00	.00	.00	.00	.00	.00	.00
20.00	-4.81	-30.85	-30.85	-4.81	-4.81	-47.39	-47.39	-4.81	20.00	.00	.00	.00	.00	.00	.00	.00	.00
30.00	-4.81	-27.04	-27.04	-4.81	-4.81	-51.90	-51.90	-4.81	30.00	.00	.00	.00	.00	.00	.00	.00	.00
40.00	-4.81	-23.33	-23.33	-4.81	-4.81	-56.63	-56.63	-4.81	40.00	.00	.00	.00	.00	.00	.00	.00	.00
50.00	-4.81	-19.68	-19.68	-4.81	-4.81	-61.47	-61.47	-4.81	50.00	.00	.00	.00	.00	.00	.00	.00	.00
60.00	-4.81	-16.17	-16.17	-4.81	-4.81	-66.71	-66.71	-4.81	60.00	.00	.00	.00	.00	.00	.00	.00	.00
70.00	-4.81	-12.75	-12.75	-4.81	-4.81	-72.09	-72.09	-4.81	70.00	.00	.00	.00	.00	.00	.00	.00	.00
80.00	-4.81	-9.42	-9.42	-4.81	-4.81	-77.89	-77.89	-4.81	80.00	.00	.00	.00	.00	.00	.00	.00	.00
90.00	-4.81	-6.44	-6.44	-4.81	-4.81	-84.05	-84.05	-4.81	90.00	.00	.00	.00	.00	.00	.00	.00	.00
100.00	-4.81	-5.00	-5.00	-4.81	-4.81	-90.54	-90.54	-4.81	100.00	.00	.00	.00	.00	.00	.00	.00	.00
110.00	-4.81	-4.93	-4.93	-4.81	-4.81	-97.81	-97.81	-4.81	110.00	.00	.00	.00	.00	.00	.00	.00	.00
120.00	-4.81	-4.85	-4.85	-4.81	-4.81	-105.07	-105.07	-4.81	120.00	.00	.00	.00	.00	.00	.00	.00	.00
130.00	-4.81	-4.78	-4.78	-4.81	-4.81	-112.07	-112.07	-4.81	130.00	.00	.00	.00	.00	.00	.00	.00	.00
140.00	-4.81	-4.71	-4.71	-4.81	-4.81	-118.80	-118.80	-4.81	140.00	.00	.00	.00	.00	.00	.00	.00	.00
150.00	-4.81	-4.64	-4.64	-4.81	-4.81	-125.32	-125.32	-4.81	150.00	.00	.00	.00	.00	.00	.00	.00	.00
160.00	-4.81	-4.57	-4.57	-4.81	-4.81	-131.91	-131.91	-4.81	160.00	.00	.00	.00	.00	.00	.00	.00	.00
170.00	-4.80	-4.50	-4.50	-4.80	-4.80	-138.49	-138.49	-4.80	170.00	.00	.00	.00	.00	.00	.00	.00	.00
180.00	-4.80	-4.42	-4.42	-4.80	-4.80	-145.42	-145.42	-4.80	180.00	.00	.00	.00	.00	.00	.00	.00	.00
190.00	-4.80	-4.35	-4.35	-4.80	-4.80	-152.45	-152.45	-4.80	190.00	.00	.00	.00	.00	.00	.00	.00	.00
200.00	-4.80	-4.28	-4.28	-4.80	-4.80	-159.96	-159.96	-4.80	200.00	.00	.00	.00	.00	.00	.00	.00	.00
210.00	-4.80	-4.21	-4.21	-4.80	-4.80	-167.72	-167.72	-4.80	210.00	.00	.00	.00	.00	.00	.00	.00	.00
220.00	-4.80	-4.14	-4.14	-4.80	-4.80	-175.80	-175.80	-4.80	220.00	.00	.00	.00	.00	.00	.00	.00	.00
230.00	-4.81	-4.06	-4.06	-4.81	-4.81	-184.22	-184.22	-4.81	230.00	.00	.00	.00	.00	.00	.00	.00	.00
240.00	-4.81	-3.99	-3.99	-4.81	-4.81	-192.65	-192.65	-4.81	240.00	.00	.00	.00	.00	.00	.00	.00	.00

SUSPENDED LINE LENGTHS (FT)								DECLINATION ANGLES AT FAIRLEAD (DEG)									
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (FT )																	
.00	2957.76	2000.00	2000.00	2957.76	2957.76	2000.00	2000.00	2957.76	.00	3.45	29.03	29.03	3.45	3.45	29.03	29.03	3.45
10.00	2957.82	2000.00	2000.00	2957.82	2957.82	2000.00	2000.00	2957.82	10.00	3.44	29.20	29.20	3.44	3.44	28.85	28.85	3.44
20.00	2957.99	2000.00	2000.00	2957.99	2957.99	2000.00	2000.00	2957.99	20.00	3.44	29.41	29.41	3.44	3.44	28.68	28.68	3.44
30.00	2958.28	2000.00	2000.00	2958.28	2958.28	2000.00	2000.00	2958.28	30.00	3.44	29.62	29.62	3.44	3.44	28.52	28.52	3.44
40.00	2958.67	2000.00	2000.00	2958.67	2958.67	2000.00	2000.00	2958.67	40.00	3.43	29.87	29.87	3.43	3.43	28.36	28.36	3.43
50.00	2959.19	2000.00	2000.00	2959.19	2959.19	2000.00	2000.00	2959.19	50.00	3.43	30.16	30.16	3.43	3.43	28.22	28.22	3.43
60.00	2959.81	2000.00	2000.00	2959.81	2959.81	2000.00	2000.00	2959.81	60.00	3.43	30.50	30.50	3.43	3.43	28.07	28.07	3.43
70.00	2960.56	2000.00	2000.00	2960.56	2960.56	2000.00	2000.00	2960.56	70.00	3.42	30.96	30.96	3.42	3.42	27.93	27.93	3.42
80.00	2961.41	2000.00	2000.00	2961.41	2961.41	2000.00	2000.00	2961.41	80.00	3.42	31.68	31.68	3.42	3.42	27.79	27.79	3.42
90.00	2962.38	2000.00	2000.00	2962.38	2962.38	2000.00	2000.00	2962.38	90.00	3.41	32.86	32.86	3.41	3.41	27.65	27.65	3.41
100.00	2963.46	1990.86	1990.86	2963.46	2963.46	2000.00	2000.00	2963.46	100.00	3.40	34.00	34.00	3.40	3.40	27.52	27.52	3.40
110.00	2964.66	1973.61	1973.61	2964.66	2964.66	2010.49	2010.49	2964.66	110.00	3.40	34.13	34.13	3.40	3.40	27.39	27.39	3.40
120.00	2965.97	1956.35	1956.35	2965.97	2965.97	2046.08	2046.08	2965.97	120.00	3.39	34.27	34.27	3.39	3.39	27.24	27.24	3.39
130.00	2967.39	1939.10	1939.10	2967.39	2967.39	2135.68	2135.68	2967.39	130.00	3.38	34.42	34.42	3.38	3.38	27.04	27.04	3.38
140.00	2968.93	1921.84	1921.84	2968.93	2968.93	2221.61	2221.61	2968.93	140.00	3.37	34.56	34.56	3.37	3.37	26.80	26.80	3.37
150.00	2970.58	1904.59	1904.59	2970.58	2970.58	2305.12	2305.12	2970.58	150.00	3.36	34.72	34.72	3.36	3.36	26.54	26.54	3.36
160.00	2972.35	1887.33	1887.33	2972.35	2972.35	2389.20	2389.20	2972.35	160.00	3.35	34.87	34.87	3.35	3.35	26.23	26.23	3.35
170.00	2974.23	1870.08	1870.08	2974.23	2974.23	2473.46	2473.46	2974.23	170.00	3.34	35.04	35.04	3.34	3.34	25.93	25.93	3.34
180.00	2976.22	1852.83	1852.83	2976.22	2976.22	2562.03	2562.03	2976.22	180.00	3.32	35.21	35.21	3.32	3.32	25.57	25.57	3.32
190.00	2978.33	1835.57	1835.57	2978.33	2978.33	2651.97	2651.97	2978.33	190.00	3.31	35.39	35.39	3.31	3.31	25.21	25.21	3.31
200.00	2980.72	1818.32	1818.32	2980.72	2980.72	2747.84	2747.84	2980.72	200.00	3.30	35.57	35.57	3.30	3.30	24.81	24.81	3.30
210.00	2983.40	1801.06	1801.06	2983.40	2983.40	2847.12	2847.12	2983.40	210.00	3.28	35.76	35.76	3.28	3.28	24.40	24.40	3.28
220.00	2986.22	1783.81	1783.81	2986.22	2986.22	2950.52	2950.52	2986.22	220.00	3.27	35.96	35.96	3.27	3.27	23.98	23.98	3.27
230.00	2989.17	1766.55	1766.55	2989.17	2989.17	3058.02	3058.02	2989.17	230.00	3.25	36.16	36.16	3.25	3.25	23.53	23.53	3.25
240.00	2992.24	1749.30	1749.30	2992.24	2992.24	3165.93	3165.93	2992.24	240.00	3.23	36.38	36.38	3.23	3.23	23.10	23.10	3.23

***** YAW OFFSET RESTORING CHARACTERISTICS *****										***** YAW OFFSET RESTORING CHARACTERISTICS *****																			
OFFSET PARITY = -1. ( C-WISE)										OFFSET PARITY = -1. ( C-WISE)																			
<b>---- MOST EXPOSED LINE CHARACTERISTICS ----</b>																													
<b>----- FAIRLEAD TENSIONS -----</b>																													
OFFSET (DEG)	LINE NO.	TOTAL (K.LBS)	HORIZ. (K.LBS)	VERT. (K.LBS)	UNSTRETCHED LENGTH (FT)	SUSPENDED PARALLEL (K.LBS)	ANCHOR FORCES REL. TO BOTTOM (K.LBS)	TOTAL YAW RESTORING MOMENT (K.LBS*FT)																					
.0	8	80.00	79.85	-4.81	2957.8	79.85	.00	0.000E+00																					
5.0	6	92.63	81.18	-44.61	2000.0	81.18	.00	0.201E+05																					
10.0	6	107.09	94.08	-51.18	2000.0	94.08	.00	0.408E+05																					
15.0	6	123.60	108.82	-58.60	2000.0	108.82	.00	0.626E+05																					
20.0	6	142.45	125.71	-67.01	2000.0	125.71	.00	0.849E+05																					
25.0	6	164.11	145.14	-76.59	2000.0	145.14	.00	0.106E+06																					
30.0	6	189.22	167.72	-87.61	2000.0	167.72	.00	0.128E+06																					
35.0	6	218.72	194.28	-100.46	2014.8	194.28	.00	0.153E+06																					
40.0	6	249.87	222.62	-113.46	2153.5	222.62	.00	0.180E+06																					
45.0	6	281.27	251.65	-125.64	2309.2	251.65	.00	0.209E+06																					
50.0	6	314.79	283.02	-137.80	2464.7	283.02	.00	0.242E+06																					
55.0	6	351.85	318.06	-150.47	2626.6	318.06	.00	0.281E+06																					
60.0	8	416.95	409.90	-76.32	4216.3	409.90	.00	0.325E+06																					
65.0	8	506.83	497.59	-96.33	4471.4	497.59	.00	0.373E+06																					
70.0	8	616.42	604.65	-119.88	4500.0	604.65	21.38	0.425E+06																					
75.0	8	751.39	736.49	-148.89	4500.0	736.49	50.39	0.479E+06																					
80.0	8	903.53	885.11	-181.53	4500.0	885.11	83.03	0.529E+06																					
TABLE RANGE EXCEEDED ON OFFSET = 85.0																													

TOTAL FAIRLEAD LINE TENSION (K.LBS)										HORIZONTAL TENSION COMPONENTS (K.LBS)									
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8		
OFFSET (DEG)	.00	80.00	80.00	80.00	80.00	80.00	80.00	80.00	OFFSET (DEG)	.00	79.85	69.95	69.95	79.85	79.85	69.95	69.95		
5.00	71.80	92.63	69.20	90.78	71.80	92.63	69.20	90.78	5.00	71.64	81.18	60.38	90.65	71.64	81.18	60.38	90.65		
10.00	65.30	107.09	59.86	103.75	65.30	107.09	59.86	103.75	10.00	65.12	94.08	52.11	103.63	65.12	94.08	52.11	103.63		
15.00	60.03	123.60	51.90	119.87	60.03	123.60	51.90	119.87	15.00	59.84	108.82	45.07	119.78	59.84	108.82	45.07	119.78		
20.00	55.82	142.45	45.48	136.85	55.82	142.45	45.48	136.85	20.00	55.61	125.71	39.42	136.72	55.61	125.71	39.42	136.72		
25.00	53.04	164.11	40.27	148.96	53.04	164.11	40.27	148.96	25.00	52.82	145.14	34.83	148.69	52.82	145.14	34.83	148.69		
30.00	50.91	189.22	36.46	163.96	50.91	189.22	36.46	163.96	30.00	50.68	167.72	31.49	163.44	50.68	167.72	31.49	163.44		
35.00	49.46	218.72	33.90	182.57	49.46	218.72	33.90	182.57	35.00	49.22	194.28	29.24	181.69	49.22	194.28	29.24	181.69		
40.00	48.69	249.87	32.57	207.24	48.69	249.87	32.57	207.24	40.00	48.45	222.62	28.07	205.78	48.45	222.62	28.07	205.78		
45.00	48.62	281.27	32.48	240.37	48.62	281.27	32.48	240.37	45.00	48.38	251.65	28.00	238.05	48.38	251.65	28.00	238.05		
50.00	49.24	314.79	33.64	284.14	49.24	314.79	33.64	284.14	50.00	49.01	283.02	29.02	280.64	49.01	283.02	29.02	280.64		
55.00	50.56	351.85	36.03	342.76	50.56	351.85	36.03	342.76	55.00	50.32	318.06	31.12	337.67	50.32	318.06	31.12	337.67		
60.00	52.55	393.49	39.65	416.95	52.55	393.49	39.65	416.95	60.00	52.32	357.73	34.28	409.90	52.32	357.73	34.28	409.90		
65.00	55.19	440.39	44.69	506.83	55.19	440.39	44.69	506.83	65.00	54.98	402.74	38.72	497.59	54.98	402.74	38.72	497.59		
70.00	59.05	490.57	50.92	616.42	59.05	490.57	50.92	616.42	70.00	58.85	451.21	44.22	604.65	58.85	451.21	44.22	604.65		
75.00	64.15	540.11	58.69	751.39	64.15	540.11	58.69	751.39	75.00	63.97	499.29	51.07	736.49	63.97	499.29	51.07	736.49		
80.00	70.18	585.06	67.80	903.53	70.18	585.06	67.80	903.53	80.00	70.01	543.12	59.13	885.11	70.01	543.12	59.13	885.11		

***** VERTICAL TENSION COMPONENTS (K.LBS) *****									***** ANCHOR PULL PERPENDICULAR TO BOTTOM (K.LBS) *****								
OFFSET PARITY = -1. ( C-WISE )									OFFSET PARITY = -1. ( C-WISE )								
LINE NO.	1	2	3	4	5	6	7	8	LINE NO.	1	2	3	4	5	6	7	8
OFFSET (DEG)									OFFSET (DEG)								
.00	-4.81	-38.82	-38.82	-4.81	-4.81	-38.82	-38.82	-4.81	.00	.00	.00	.00	.00	.00	.00	.00	.00
5.00	-4.81	-44.61	-33.82	-4.82	-4.81	-44.61	-33.82	-4.82	5.00	.00	.00	.00	.00	.00	.00	.00	.00
10.00	-4.82	-51.18	-29.46	-4.81	-4.82	-51.18	-29.46	-4.81	10.00	.00	.00	.00	.00	.00	.00	.00	.00
15.00	-4.82	-58.60	-25.72	-4.81	-4.82	-58.60	-25.72	-4.81	15.00	.00	.00	.00	.00	.00	.00	.00	.00
20.00	-4.81	-67.01	-22.68	-5.87	-4.81	-67.01	-22.68	-5.87	20.00	.00	.00	.00	.00	.00	.00	.00	.00
25.00	-4.83	-76.59	-20.21	-8.97	-4.83	-76.59	-20.21	-8.97	25.00	.00	.00	.00	.00	.00	.00	.00	.00
30.00	-4.83	-87.61	-18.38	-13.00	-4.83	-87.61	-18.38	-13.00	30.00	.00	.00	.00	.00	.00	.00	.00	.00
35.00	-4.83	-100.46	-17.15	-17.97	-4.83	-100.46	-17.15	-17.97	35.00	.00	.00	.00	.00	.00	.00	.00	.00
40.00	-4.83	-113.46	-16.51	-24.56	-4.83	-113.46	-16.51	-24.56	40.00	.00	.00	.00	.00	.00	.00	.00	.00
45.00	-4.83	-125.64	-16.47	-33.27	-4.83	-125.64	-16.47	-33.27	45.00	.00	.00	.00	.00	.00	.00	.00	.00
50.00	-4.83	-137.80	-17.03	-44.46	-4.83	-137.80	-17.03	-44.46	50.00	.00	.00	.00	.00	.00	.00	.00	.00
55.00	-4.83	-150.47	-18.18	-58.89	-4.83	-150.47	-18.18	-58.89	55.00	.00	.00	.00	.00	.00	.00	.00	.00
60.00	-4.83	-163.90	-19.91	-76.32	-4.83	-163.90	-19.91	-76.32	60.00	.00	.00	.00	.00	.00	.00	.00	.00
65.00	-4.81	-178.15	-22.30	-96.33	-4.81	-178.15	-22.30	-96.33	65.00	.00	.00	.00	.00	.00	.00	.00	.00
70.00	-4.82	-192.54	-25.26	-119.88	-4.82	-192.54	-25.26	-119.88	70.00	.00	.00	.00	21.38	.00	.00	.00	21.38
75.00	-4.82	-205.97	-28.91	-148.89	-4.82	-205.97	-28.91	-148.89	75.00	.00	.00	.00	50.39	.00	.00	.00	50.39
80.00	-4.80	-217.51	-33.17	-181.53	-4.80	-217.51	-33.17	-181.53	80.00	.00	.00	.00	83.03	.00	.00	.00	83.03

***** SUSPENDED LINE LENGTHS (FT) *****									***** DECLINATION ANGLES AT FAIRLEAD (DEG) *****												
LINE NO.		1	2	3	4	5	6	7	8	LINE NO.		1	2	3	4	5	6	7	8		
OFFSET (DEG)		.00	2957.76	2000.00	2000.00	2957.76	2957.76	2000.00	2000.00	2957.76	OFFSET (DEG)		.00	3.45	29.03	29.03	3.45	3.45	29.03	29.03	3.45
5.00	2898.32	2000.00	2000.00	3029.37	2898.32	2000.00	2000.00	3029.37		5.00	3.84	28.79	29.25	3.04	3.84	28.79	29.25	3.04			
10.00	2850.60	2000.00	2000.00	3113.84	2850.60	2000.00	2000.00	3113.84		10.00	4.23	28.55	29.48	2.66	4.23	28.55	29.48	2.66			
15.00	2811.11	2000.00	2000.00	3213.69	2811.11	2000.00	2000.00	3213.69		15.00	4.60	28.30	29.71	2.30	4.60	28.30	29.71	2.30			
20.00	2779.12	2000.00	2000.00	3307.01	2779.12	2000.00	2000.00	3307.01		20.00	4.94	28.06	29.91	2.46	4.94	28.06	29.91	2.46			
25.00	2757.00	2000.00	2000.00	3351.18	2757.00	2000.00	2000.00	3351.18		25.00	5.22	27.82	30.12	3.45	5.22	27.82	30.12	3.45			
30.00	2740.09	2000.00	2000.00	3404.33	2740.09	2000.00	2000.00	3404.33		30.00	5.45	27.58	30.27	4.55	5.45	27.58	30.27	4.55			
35.00	2728.54	2014.81	2000.00	3469.07	2728.54	2014.81	2000.00	3469.07		35.00	5.60	27.34	30.39	5.65	5.60	27.34	30.39	5.65			
40.00	2722.45	2153.47	2000.00	3553.77	2722.45	2153.47	2000.00	3553.77		40.00	5.69	27.01	30.46	6.81	5.69	27.01	30.46	6.81			
45.00	2721.88	2309.16	2000.00	3665.28	2721.88	2309.16	2000.00	3665.28		45.00	5.70	26.53	30.47	7.96	5.70	26.53	30.47	7.96			
50.00	2726.83	2464.68	2000.00	3808.74	2726.83	2464.68	2000.00	3808.74		50.00	5.63	25.96	30.40	9.00	5.63	25.96	30.40	9.00			
55.00	2737.27	2626.62	2000.00	3993.32	2737.27	2626.62	2000.00	3993.32		55.00	5.48	25.32	30.29	9.89	5.48	25.32	30.29	9.89			
60.00	2753.08	2798.42	2000.00	4216.29	2753.08	2798.42	2000.00	4216.29		60.00	5.27	24.62	30.14	10.55	5.27	24.62	30.14	10.55			
65.00	2774.15	2980.59	2000.00	4471.36	2774.15	2980.59	2000.00	4471.36		65.00	5.00	23.86	29.94	10.96	5.00	23.86	29.94	10.96			
70.00	2803.71	3164.54	2000.00	4500.00	2803.71	3164.54	2000.00	4500.00		70.00	4.68	23.11	29.74	11.21	4.68	23.11	29.74	11.21			
75.00	2842.00	3336.34	2000.00	4500.00	2842.00	3336.34	2000.00	4500.00		75.00	4.31	22.42	29.51	11.43	4.31	22.42	29.51	11.3			
80.00	2886.82	3483.85	2000.00	4500.00	2886.82	3483.85	2000.00	4500.00		80.00	3.93	21.83	29.29	11.59	3.93	21.83	29.29	11.59			

